Modified Rhie-Chow/PISO Algorithm for Collocated Variable Finite Volume Porous Media Flow Solvers

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# Outline



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- 3 Analysis of pressure-velocity coupling algorithm
- 4 Modified Rhie-Chow/PISO Algorithm
- 5 Validation of proposed algorithm

### 6 Conclusions

# Background

• Flow simulations performed using standard segregated algorithms and interpolation schemes on collocated grids generates spurious oscillations in the velocity near porous interfaces



# Background

- Flow simulations performed using standard segregated algorithms and interpolation schemes on collocated grids generates spurious oscillations in the velocity near porous interfaces
- Especially for high Reynolds number flows or for low permeability heterogeneous porous media



# Objective

# To develop a modified Rhie-Chow / $\mathsf{PISO}^1$ segregated algorithm for low Mach number flow in heterogeneous, isotropic porous media



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<sup>1</sup>PISO = Pressure-Implicit with Splitting of Operators  $\overline{}$ 

Modified Rhie-Chow/PISO Algorithm .

# Objective

# To develop a modified Rhie-Chow / $PISO^1$ segregated algorithm for low Mach number flow in heterogeneous, isotropic porous media, which by construction avoids the development of spurious oscillations



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 $^{1}$ PISO = Pressure-Implicit with Splitting of Operators

Modified Rhie-Chow/PISO Algorithm .

# Analysis of pressure-velocity coupling algorithm

#### to understand the origin of the pressure-velocity decoupling resulting in spurious oscillations



# Governing equations

Analysis of pressure-velocity decoupling

Volume averaged conservation equations for compressible flow and heat transfer in porous media under thermal non-equilibrium



# Governing equations

Analysis of pressure-velocity decoupling

Volume averaged conservation equations for compressible flow and heat transfer in porous media under thermal non-equilibrium

- Mass conservation:
- Momentum conservation:

 $\partial_t (\phi \langle \rho_\alpha \rangle^\alpha) + \partial_i (\langle \rho_\alpha \rangle^\alpha \langle u_i \rangle) = 0$ 

$$\begin{aligned} \partial_t (\langle \rho_\alpha \rangle^\alpha \langle u_i \rangle) + \partial_j (\phi^{-1} \langle \rho_\alpha \rangle^\alpha \langle u_j \rangle \langle u_i \rangle) &= \\ -\phi \partial_i \langle p_\alpha \rangle^\alpha + \partial_j \langle \tau_{ij} \rangle + \phi \langle f_i \rangle^\alpha - \phi D \langle u_i \rangle \end{aligned}$$

• Fluid energy conservation:  

$$\langle c_{\rho,\alpha} \rangle^{\alpha} \left( \partial_{t} (\phi \langle \rho_{\alpha} \rangle^{\alpha} \langle T_{\alpha} \rangle^{\alpha}) + \partial_{i} (\langle \rho_{\alpha} \rangle^{\alpha} \langle u_{i} \rangle \langle T_{\alpha} \rangle^{\alpha}) \right) = \partial_{i} (\lambda_{\alpha}^{e} \partial_{i} \langle T_{\alpha} \rangle^{\alpha})$$

$$+ h_{\alpha\beta} a_{\alpha\beta} (\langle T_{\beta} \rangle^{\beta} - \langle T_{\alpha} \rangle^{\alpha}) + \partial_{t} (\phi \langle \rho_{\alpha} \rangle^{\alpha}) + \langle u_{i} \rangle \partial_{i} \langle \rho_{\alpha} \rangle^{\alpha}$$

Solid energy conservation:

$$\begin{split} \langle \boldsymbol{c}_{\boldsymbol{p},\beta} \rangle^{\beta} \langle \boldsymbol{\rho}_{\beta} \rangle^{\beta} \partial_{t} ((1-\phi) \langle \boldsymbol{T}_{\beta} \rangle^{\beta}) &= \partial_{i} (\lambda_{\beta}^{\boldsymbol{e}} \partial_{i} \langle \boldsymbol{T}_{\beta} \rangle^{\beta}) \\ &- \boldsymbol{h}_{\alpha\beta} \boldsymbol{a}_{\alpha\beta} (\langle \boldsymbol{T}_{\beta} \rangle^{\beta} - \langle \boldsymbol{T}_{\alpha} \rangle^{\alpha}) \end{split}$$



Analysis of pressure-velocity decoupling Assume isothermal case for demonstration



Analysis of pressure-velocity decoupling

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Predictor step:

**Solve discretized momentum equation**  $A_P u_{i,P} = H_{i,P} - \phi_P V_P^{-1} \sum_f p_f S_{i,f}$ 





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- Orrector steps:
  - ► Solve discretized pressure equation  $V_P \partial_t (\phi_P \psi_P p_P) + \sum_f (\rho A^{-1} H_i)_f S_{i,f} = \sum_f (\rho A^{-1} \phi \partial_i p)_f S_{i,f}$





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  - Correct velocity  $u_{i,P} = A_P^{-1}(H_{i,P} - \phi_P V_P^{-1} \sum_f p_f S_{i,f})$

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  - ► Update mass flux at faces  $(\rho u_i)_f S_{i,f} = (\rho A^{-1} H_i)_f S_{i,f} - (\rho A^{-1} \phi)_f (\partial_i \rho)_f S_{i,f}$
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#### Interpolation from cell- to face-centers required

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Analysis of pressure-velocity decoupling

- Flow in a 1D heterogeneous porous medium:
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### Analytical solution:

- Constant velocity
- Linear pressure drop in porous medium



Analysis of pressure-velocity decoupling

#### Example of decoupling:

• Solving of momentum conservation equation in the predictor step:

$$A_P u_{i,P} = H_{i,P} - \phi_P V_P^{-1} \sum_f p_f S_{i,f}$$



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Analysis of pressure-velocity decoupling

Other examples of decoupling due to inconsistent interpolation of discontinuous terms to the faces

- Pressure equation in the corrector step, since A also includes  $\phi$  $V_P \partial_t (\phi_P \psi_P p_P) + \sum_f (\rho A^{-1} H_i)_f S_{i,f} = \sum_f (\rho A^{-1} \phi)_f (\partial_i p)_f S_{i,f}$
- Velocity correction:  $u_{i,P} = A_P^{-1}(H_{i,P} - \phi_P V_P^{-1} \sum_f p_f S_{i,f})$



# Modified Rhie-Chow/PISO Algorithm for Collocated Variable Finite Volume Porous Media Flow Solvers

#### Redistributed Resistivity PISO (rdrPISO) algorithm



# Key elements of algorithm

Redistributed Resistivity PISO algorithm

#### Key elements:

- Modified momentum / velocity corrections equation
- Ø Modified pressure equation (Rhie-Chow interpolation)

to ensure strong velocity-pressure coupling close to discontinuities



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Cell-centered pressure gradients are not correctly balanced by the resistivity, in neighboring cells to the interface



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- Reformulation of momentum equation to avoid:
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  - having the resistivity as part of  $A_P$  and  $H_{i,P}$
- Redistribution of resistivity to balance the cell-centered pressure gradients in neighboring cells to the discontinuity



Reformulation of momentum equation

- $\bullet\,$  Divide momentum equation by  $\phi\,$
- $\bullet\,$  Move  $\phi^{-1}$  out of convection term

so that no explicit interpolation of porosity is required for the discretization of the momentum equation  $\label{eq:constraint}$ 

$$\frac{1}{\phi_P}\partial_t(\rho_P u_{i,P}) + \frac{1}{\phi_P^2 V_P}\sum_f (\rho u_j)_f u_{i,f}S_{j,f} = -(\partial_i p)_P + \frac{1}{\phi_P V_P}\sum_f \tau_{ij,f}S_{j,f} + f_{i,P} - D_P u_{i,P}$$



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• Keep resistivity term outside of  $A_P$  and  $H_{i,P}$ 

$$(A_P + D_P)u_{i,P} = H_{i,P} - V_P^{-1} \sum_f p_f S_{i,f}$$

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to balance the cell-centered pressure gradient calculated with central differences (same stencil)



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Modified momentum equation

$$(A_{P}+D_{P}^{rd})u_{i,P}=H_{i,P}-V_{P}^{-1}\sum_{f}p_{f}S_{i,f}$$



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Modified momentum equation  $(A_P + D_P^{rd})u_{i,P} = H_{i,P} - V_P^{-1} \sum_f p_f S_{i,f}$ 



Modified velocity correction equation

$$u_{i,P} = (A_P + D_P^{rd})^{-1} (H_{i,P} - V_P^{-1} \sum_f p_f S_{i,f})$$

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Redistributed Resistivity PISO algorithm

#### Cause for decoupling:

Inconsistent interpolation of discontinuous terms to the faces in the standard pressure equation, since A also includes  $\phi$ 

 $V_P \partial_t (\phi_P \psi_P p_P) + \sum_f (\rho A^{-1} H_i)_f S_{i,f} = \sum_f (\rho A^{-1} \phi)_f (\partial_i p)_f S_{i,f}$ 



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- Reformulation of **semi-discretized** momentum equation to avoid:
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- Reformulation of semi-discretized momentum equation to avoid:
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  - having the resistivity as part of A and  $H_i$
- Modification of Rhie-Chow interpolation to ensure consistent interpolation of discontinuous coefficients in pressure equation

Redistributed Resistivity PISO algorithm

#### Reformulation of semi-discretized momentum equation

- $\bullet\,$  Divide momentum equation by  $\phi\,$
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$$u_{i,P} = \mathbf{B}_{P}(A_{P}^{-1}H_{i,P} - A_{P}^{-1}(\partial_{i}p)_{P})$$

where  $B_P = (1 + D_P A_P^{-1})^{-1}$ 



# Modified pressure equation Redistributed Resistivity PISO algorithm

#### Modification of Rhie-Chow interpolation

• Express the mass flux through a face as:

$$(\rho u_i)_f S_{i,f} = \frac{B_f[(\rho A^{-1} H_i)_f S_{i,f} - (\rho A^{-1})_f (\partial_i p)_f S_{i,f}]}{(\rho A^{-1} H_i)_f S_{i,f}}$$

instead of:  $(\rho u_i)_f S_{i,f} = (\rho B A^{-1} H_i)_f S_{i,f} - (\rho B A^{-1} \partial_i p)_f S_{i,f}$ where  $B_f = (1 + D_f (A^{-1})_f)^{-1}$ 



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• Modified pressure equation:

$$V_P \partial_t (\phi_P \psi_P p_P) + \sum_f \frac{B_f (\rho A^{-1} H_i)_f S_{i,f}}{S_{i,f}} = \sum_f \frac{B_f (\rho A^{-1})_f (\partial_i p)_f S_{i,f}}{S_{i,f}}$$



Redistributed Resistivity PISO algorithm

Assume isothermal case for demonstration



Redistributed Resistivity PISO algorithm

Assume isothermal case for demonstration

Update and redistribute resistivity: Compute D<sub>P</sub>, D<sub>f</sub>, D<sub>P</sub><sup>rd</sup> and D<sub>f</sub><sup>rd</sup>



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Solve modified discretized momentum equation  $(A_P + D_P^{rd})u_{i,P} = H_{i,P} - V_P^{-1} \sum_f p_f S_{i,f}$ 



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  - Correct velocity:  $u_{i,P} = (A_P + D_P^{rd})^{-1} (H_{i,P} - V_P^{-1} \sum_f p_f S_{i,f})$

# Validation of proposed algorithm





# Porous plug case

#### Validation of proposed algorithm



# Porous plug case

#### Validation of proposed algorithm



Centerline velocity for  $Re \in [10^2, 10^3]$ , and  $Da \in [10^{-3}, 10^{-7}]$ 

# Beaver-Joseph case

#### Validation of modified algorithm





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- Successfully validated for incompressible and isothermal flow parallel and perpendicular to porous regions



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- Successfully validated for incompressible and isothermal flow parallel and perpendicular to porous regions
- Robustness demonstrated for high Re flows up to  $Re = 10^3$  and for Da numbers as low as  $Da = 10^{-7}$



# Thank you for your attention!

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